CHAPTER E INTERCHANGES

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CHAPTER E INTERCHANGES

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E.1 GENERAL

Interchanges are relatively complex and have many components which need to be designed to suit the through and connecting highways as well as the traffic volumes, speed, rural or urban settings and any constraints imposed by the physical environment. This manual does not deal comprehensively with the subject of interchanges.

In Alberta, the conceptual or functional design of interchanges that identifies the configuration and general layout, is normally done at the planning stage. This sometimes involves identifying several stages of development for the interchange. As planning work is often done many years in advance of design, there is a need to review the technical details of a planning study to ensure that current design vehicles, speeds and practices have been used. Much of that information is contained in other chapters of this manual.

E.2 RAMPS

For detailed design of interchanges, designers may use the drawings contained in this chapter for layout of on-ramps and off-ramps on the through highway.

E.2.1 Exit Terminal Design

For single lane exit terminals, either the direct taper (as shown on Figure E-1.3) or a parallel lane design (not shown here) may be used. In the parallel lane design, a short taper is used to develop a lane of constant width for some distance gradually widening at the nose. Exiting vehicles are expected to change lanes and decelerate without impeding the through traffic. This type of layout offers some advantages when the exit terminal is located on or under a structure (effectively reducing the length of structure required compared to the direct taper design).

In the direct taper design, the right edge of the ramp terminal gradually widens from the beginning of the ramp terminal to the nose. Exiting vehicles are expected to maintain close to full speed until they are entirely off the through lanes to avoid impeding through traffic.

E.2.2 Entrance Terminal Design

Single lane entrance ramps may be either direct taper design (as shown in Figure E.1.2) or parallel lane design (not shown). In the parallel lane design, an auxiliary lane of constant width is added to the right of the through lanes and is discontinued, by means of a taper, some distance downstream. The driver entering a parallel lane is expected to accelerate to a suitable speed before merging with through traffic. The parallel lane design offers some advantages (lower capital costs) where the entrance terminal is located on top of or under a structure.

The direct taper layout provides a uniform taper from the entrance nose to the edge of through lane. The taper rate is chosen to allow vehicles entering the highway to accelerate to close to the through traffic speed before having to merge.

Two lane entrance ramps may be of the direct taper or parallel type design.

E.2.3 Ramp Junctions

On the intersecting highway or roadway, the junction with the ramp may be treated as a stop condition (for example at a diamond interchange) or as a free flow merge condition (for example at a cloverleaf interchange) as per the planning study. The design and layout of these terminals should be suitable for the traffic as well as being consistent with previous Alberta practice for this type of junction. The layout should be suitable for the turning template of all appropriate design vehicles.

E.3 REFERENCE DOCUMENTS

As this Design Guide does not fully cover the subject of Interchange Design, designers are referred to the following documents for additional information.

- Geometric Design Guide For Canadian Roads (1986) – TAC
- Urban Supplement to the Geometric Design Guide for Canadian Roads (1995) – TAC
- A Policy on Geometric Design of Highways and Streets (1994) AASHTO
- Highway Capacity Manual (1994) FHWA

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* DECELERATION BEGINS AFTER TAPERED LANE IS 3.7m WIDE AND RATE OF DECELERATION IS COMFORTABLE, (NO BRAKING REQUIRED).

	FAC	ILITY	DESI	GN WARRAN	ITS		EXIT TE	RMINAL FF	ROM HIGHWA	AY (SEE FIGU	RE E-1.3)				ENTRANCE	TERMINAL	TO HIGHWA	Y (SEE FIC	SURE E-1.2)			NO	<u>'E:</u>											
	MAIN SPE	LINE EED	С	ONTROLLING RADIUS m	SPE AT G((IIm OF (km	ED DRE FSET) /h)	DE SIGN CRITE (GRADE - 3	RIA (NORMAL m) 3% TO +3%	_) -3% to	DESIGN CRI O -5% -5%	TERIA FOR GR/ VER 3% (m) +3% TO	ADIENTS A	SPEEI 2m OF (km/	DAT DESI FSET	IGN CRITERIA (NG (m) GRADE -3% TO	ORMAL) +3%	-3% TO -5	DE SIGN CR C % -5%	ITERIA FOR GRADIENTS IVER 3% (m) +3% TO +5%	<u>^</u> +5%		WE AT REC	AVING LENGT THE DIVERGE DUIRED. GENE	H IS MEASUR ARE 3.7m RALLY AUXIL	RED FROM A APART, AS IL IARY LANES	POINT WHEF LUSTRATED A ARE USED W	RE LANE EDA ABOVE. AN A HERE THE A	GES AT THE AUXILIARY LAN WEAVING LEN	MERGE ARE IE TO ACCOM GTH IS LESS	0.5m APART ODATE WEAVI THAN 1000m	TO WHERE ING MAY BE n.	LANE EDGES ADDED WHE	S RE	
Let a let	UESIGN SPEED TYPICAL POSTED SPEED	85th PERCENTILE RUNNING SPEED ALBERTA 1989 DESILPAD	FOR RAMPS MINIMUM PAGE	FOR TAMPS DESIRABLE RADIUS FOR LOOP MINIMUM RADIUS	20% REDUCTION OF RUNNING SEC	LANE LENG BEGINNING FOR	OFFSET AT PHYSICAL GORE GORE PHYSICAL GORE PHYSICAL GORE	TO W.UM OFFSET) DIVERGE DISTANCE D' FROM 2m PANTESET TO	(Gm OFFSET) TAPER RATIO DECELERATION FVIE AT	TAPER RATIO DECELERATION DECELERATION LANE EXIT TERMINA	TAPER RATIO DECELERATION DECELERATION LANE EXIT TERMINIC	TAPER RATIO DECELERATION DECELERATION LANE EXIT TERMINIO	DESIRABLE RUNNING SPEED Bkm/h LESS	ACCELERATION LAN ACCELERATION LANE FSET AT PHYSICAL GORE TO END	LENGTH OF PAINTED WEDGE FROM PHYSICAL GORE (IOM DFFSET) TO PAINTED GORE POINT (5.3m OFFSET).	VERGE DISTANCE 'M' FROM 5.75m TO 2m OFFSET	FOR APER RATIO ACCELERATIO LANE AT ENTRANCE TERMINAL	FOR ACCELERATIO ACCELERATION LANE AT ENTRANCE TERNINN	FOR ACCELERATIO LAPER RATIO LANE AT ENTRANCE TERMINAL FOR RATIO	FOR ACCELERATIO LANE AT ENTRANCE TERMINAL	40 km/h MINIMUM R55	CONT	ROLLING	RADIUS "A" PARA 55 km/h MINIMUM RIIO	- BASE	D ON DE REQUIREN 65 km/h MINIMUM RI 60	SIGN SP MENTS - 70 km/h MINIMUM R I 90	EED OF FOR E	TURNING (IT AND E 80 km/h MINIMUM R250	ROADWA ENTRANCE 90 km/h MINIMUM R340	TERMII	MAINLINE NALS 'h / 110 km/ MINIMUM R600	ROADWA	Y 'h / 130 km/t MINIMUM R950
km/	/h km/h	km/h n	n m	m m	km/h	m	m	m	m	m	m	m	km/h	m	m	m	m	m	m	m	e=0.06	e=0.06	e=0.06	e=0.06	e=0.06	e=0.06	e=0.06	e=0.06	e=0.06	e=0.06	e=0.06	e=0.06	e=0.06	e=0.06
60	0 50	60 9	0 55	5 55 55	48	165@I	5:1 42.0	60	220 @ 20:1	20:1	15:1	15:1	60 52	200@20:1	94	75	200 @ 20:I	20:1	25:1 3	30:1	P=3.205 0=32.345 60 Lc=64.430 Ls=65.455	P=2.154 0=29.993 65 Lc=59.860 Ls=60.357	P=1.801 0=31.125 75 Lc=62.166 Ls=62.500	P=1.629 0=32.744 85 Lc=65.422 Ls=65.682	P=1.242 0=31.094 90 Lc=62.149 Ls=62.308	P=1.016 0=31.210 Lc=62.394 Ls=62.500	P=0.889 Q=31.812) Lc=63.605 Ls=63.684	P=0.869 0=33.461 2 () Lc=66.904 Ls=66.977	P=1,024 0=39,168 4 () Lc=78,314 Ls=78,400	P=0.694 0=37.632 60 Lc=75.253 Ls=75.294	P=0.706 0=43.161 95 Lc=86.313 Ls=86.350	P=0.587 0=45.973 235 Lc=91.939 Ls=91.963	P=0.525 0=48.593 270 Lc=97.182 Ls=97.200	P=0.420 0=48.940 305 Lc=97.877 Ls=97.889
80) 70	80 19	90 55	5 55 55	64	220@2	D:1 56.0	80	275 @ 25:1	25:1	20:1	15:1	79 71	≥ R90 200@20:1 R55-R90 250@25:1	94 117.5	75 93.75	250 @ 20:I	20:1	≥ R90 ≥ 30:1 3 R55-R90 R55 35:1 2	R90 35: I 5-R90 40: I	P=5.874 0=43.589 70 Lc=86.520 Ls=89.091	P=3.799 0=39.741 75 Lc=79.187 Ls=80.357	P=2.328 0=35.371 80 Lc=70.619 Ls=71.111	85	90	100	110	120	140	160	195	235	270	305
10	0 90	100 25	50 90	90 55	80	220@2	D:1 56.C	80	275 @ 25:1	25:1	20:1	15:1	95 88	≥ RI30 350@35:1 R55-RI30 400@40:1	164.5 188	131.25 150	350 @ 35:I	35:1	≥ R130 ≥ 1 50:1 6 R55-130 60:1	R130 50:1	P=12.427 0=62.679 85 Lc=123.224 Ls=131.364	P=7.778 0=56.564 90 Lc=II2.239 Ls=II5.714	P=4.604 0=49.625 95 Lc=98.901 Ls=100.278	P=3.III 0=45.I97 ()() Lc=90.221 Ls=90.909	P=2.764 0=46.340 () Lc=92.548 Ls=93.007	P=2.103 0=44.882 2 () Lc=89.684 Ls=90.000	P=1,481 0=41,054 25 Lc=82.066 Ls=82.237	P=1,196 0=39,258 30 Lc=78,488 Ls=78,605	140	160	195	235	270	305
11	0 100	109 34	40 30	90 55	87	275@2	5:1 70.0	100	330 @ 30:1	35:1	25:1	20:1	102 94	≥ RI60 500@50: I R55-RI60 550@55: I	235 258.5	187.5 206.25	400 @ 40:I	40:1	DUE TO THE LONG DIST. REQUIRED FOR ACCELER	ANCES	85	90	95	100	110	120	125	130	140	160	195	235	270	305
120	0 100	112.5 44	10 30	90 70	90	275@2	5:1 70.0	100	330 @ 30:1	35:1	25:1	20:1	109 10	≥ RI90 500@50:1 R70-R190 600@60:1	235 282	187.5 225	500 @ 50:I	40:1	GIVEN TO REDUCING MAI GIVEN TO REDUCING MAI GRADIENT, OR PROVIDING PARALLEL ACCELERATION SUCH THAT VEHICLES OF A MINIMUM SPEED OF LESS THAN PININING SE	INLINE A N LANE. BTAIN 8km/h PEED	×	P=9.600 0=62.684 95 Lc=124.134 Ls=128.929	P=5.638 0=54.857 ()() Lc=109.241 Ls=111,111	P=4.543 0=54.545 () Lc=108.783 Ls=110.000	P=3.907 0=55.051 2 () Lc=109.373 Ls=110.769	P=2.475 0=48.677 25 Lc=97.257 Ls=97.656	P=1,732 0=44.393 30 Lc=88.731 Ls=88.947	P=1.608 0=45.513 4() Lc=90.981 Ls=91.163	P=1.348 0=44.951 50 Lc=89.870 Ls=90.000	160	195	235	270	305
130	0 110	116 44	10 90	0 90 90	93	330@3	0:1 84.C	120	385 @ 35:I	440@40:1	30:1	25:1	11610	≥ R2I5 500@50:1 R90-R215 600@60:1	235 282	187.5 225	500 @ 50:I	40:1	OF THE MAINLINE BEFC MERGING SEE CHAPTER THIS MANUAL FOR TYPIC VEHICLE PERFORMANCE CHARACTERISTICS.	DRE D OF CAL	×	×	100	110	120	125	130	140	150	160	195	235	270	305

FOR TAPER DIMENSIONS, REFER TO FIGURE E-1.3

FOR TAPER DIMENSIONS, REFER TO FIGURE E-I.2

NOT	Έ:	
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ASSUMED SPEED PROFILE AT EXIT TERMINALS (ALBERTA) CONTROLLIN 85th PERCENTILE SPEED LENGTH OF TAPER SPEED AT DE SIGN NORMAL RADIUS RUNNING SPEED AT 3.7m AVAILABLE FOR SPEED TAPER km/h RATIO IIm OFFSET (GORE) (ALBERTA) OFFSET DECELERATION (20% REDUCTION) km/h (7.3m x RATIO) km/h PEED 60 60 60 109.5 15:1 48 80 20:1 80 80 146 64 ED SHO 100 100 20:1 100 146 80 109 182 SPI SPI 10 25:1 109 87 120 25:1 112.5 112.5 182 90 Zű 130 30:1 116 116 219 93

IT IS ASSUMED THAT VEHICLES EXITING THE HIGHWAY WILL MAINTAIN THE MAINLINE SPEED (85th PERCENTILE RUNNING SPEED) UNTIL THE POINT WHERE THE TAPERED LANE IS 3.7m WIDE. AT THE GORE POINT (II.Om OFFSET), IT IS ASSSUMED THAT VEHICLES HAVE SLOWED DOWN TO 80% OF THE MAINLINE SPEED. THIS DECELERATION RATE IS VERY GRADUAL AND CAN GENERALLY BE ACHIEVED BY STANDARD TRANSMISSION VEHICLES IN GEAR WITHOUT BRAKES BEING APPLIED. THE SPIRAL LENGTHS ARE DESIGNED TO ALLOW A COMFORTABLE TRANSITION TO THE CONTROLLING SPEED OF THE CIRCULAR CURVE. GENERALLY ON RAMPS WHERE THE RAMP DESIGN SPEED EXCEEDS 70 km/h, THE REDUCTION IN SPEED ON THE TRANSITION IS VERY GRADUAL AND CAN BE ACHIEVED WITHOUT BRAKING. HOWEVER, WHERE CONSTRAINTS EXIST, FOR EXAMPLE AT LOOP EXITS WITH DESIGN SPEEDS LESS THAN 70 km/h, THE DESIGN LENGTH PROVIDES FOR COMFORTABLE BRAKING. ALTHOUGH SOME BRAKING IS REQUIRED ON APPROACHES TO LOOPS, THE RATE OF DECELERATION IS GENERALLY LESS THAN HALF THAT REQUIRED ON THE APPROACH TO TURNING ROADWAYS AT CHANNELIZED INTERSECTIONS AND IS WELL WITHIN THE RANGE OF COMFORTABLE BRAKING

•NOTES: I. THE AVERAGE 85th PERCENTILE RUNNING SPEED RECORDED FOR PASSENGER VEHICLES ON FOUR LANE DIVIDED HIGHWAYS IN ALBERTA IN 1989 WAS 116 km/h WHERE THE POSTED SPEED WAS 110 km/h IN DAYTIME. THE CORRESPONDING SPEED WAS 109 km/h WHERE THE POSTED SPEED WAS 100 km/h.

2. FOR TYPICAL PAVEMENT MARKINGS FOR INTERCHANGE RAMPS REFER TO THE TRAFFIC CONTROL STANDARDS MANUAL. A RUNNING SPEED OF 112.5 km/h IS USED HERE IN CONJUNCTION WITH A 120 km/h DESIGN SPEED IN ORDER TO PROVIDE SOME INTERMIDIATE VALUES.

A	REVISED DIMENSIONS		TG	07/99						
	REVISED NOTE ·	TDN	06/98							
No.	REVISIONS		BY	DATE						
1.		FIGURE E-I.I								
		Date: APRIL 1995								
DESIGN STANDARDS OF EXIT & ENTRANCE TERMINALS FOR DIVIDED HIGHWAYS AT INTERCHANGES										
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