

ALBERTA TRANSPORTATION GEOHAZARD ASSESSMENT PROGRAM PEACE REGION – GRANDE PRAIRIE DISTRICT 2020 INSPECTION



THURBER ENGINEERING LTD.

Site Number	Location		Na	ame			Hwy	km	
GP031	South slope of the Peace River Valley near the Shaftesbury ferry crossing		Shaftesbury Slide, South Site			te	740:02	49.3	
Legal Description	1		U	TM Co-ord	nates (NAD 8	3)	•		
LSD 4-9-82-23-W		11	11U N 6 216 300			E 466 120			
	Data					T - (- 1			
Provious Inspection:				15	CF ○	120			
Current Inspection:		June 11 2020)	10	1		10		
Road AADT:		160)	10	Year:	2019			
Inspected By:		Don Proudfoot (Ed Szmata, Roc	on Proudfoot (Thurber) d Szmata, Rocky Wang (AT)						
Report Attachments:		Photograp	Photographs 🔽 Plans				Maintenance Items		
Primary Site Iss	A landslide 70 m width. of the road the backsca terrace whe The backsla slumping.	A landslide was affecting the original alignment of the highway over a 70 m width. A pile wall which had been constructed along the shoulder of the road failed and the highway was shifted onto a detour around the backscarp of the slide. The slide extended down the slope to the terrace where Range Road No.234 is located 35 m below the highway. The backslope, which was about 7 m high, had also been subject to slumping.							
Dimensions:		The main s affecting th the main sli	The main slide was 70 m wide along the highway. Three slumps were affecting the backslope over a combined width of about 80m, west of the main slide.						
History and Date of any Remediation:		The origina 2009. It con anchors (Cl were 22 m The tie-back had droppe against the The wall fai side and th backscarp of In the summ and prepar options for constructed highway in inclination, constructing highway.	The original slide occurred in 2007. A pile wall was completed in 2009. It consisted of 114 driven steel HP310x79 piles and 45 screw anchors (Chance anchors). The piles along the main section of the wall were 22 m long while the "wing wall" piles at each end were 15 m long. The tie-back anchors were 25 m long. Prior to the slide the highway had dropped and was built back up behind the wall with a MSE zone against the wall and granular subbase further away from the wall. The wall failed in July 2014 due to loss of soil support on the downslope side and the highway was shifted onto a gravel detour behind the backscarp of the slide. In the summer of 2017, Thurber conducted a geotechnical investigation and prepared a preliminary engineering assessment with design options for the repair of the landslide. The selected design, which was constructed in 2018 and 2019, consisted of a realignment of the highway into the hillside, cutting back the backslope to a flatter inclination, constructing a toe berm to buttress the highway slope and constructing a concrete pile wall along the downslope shoulder of the						
Maintenance: Maintenan stabilizatio			ce has not been required since the construct				constructio	of the latest	
Observations:				Des	cription			Worse?	
Pavement Distress									

Slope Movement	A small slump has formed in the cut slope above the west riprap channel	2
Erosion	There is evidence of erosion outside the project limits resulting in silt accumulating in a low spot in the southwest highway ditch	
✓ Seepage	There was a steady drip coming from the drainpipe indicating the presence of groundwater	
Bridge/Culvert Distress		
✓ Other	Some excess Class 1M riprap was stockpiled along the toe of the toe berm and is available for future repairs when needed	

Instrumentation:

4 slope inclinometers were installed in the pile wall and have measured deflections as follows:

- SI18-P10 = 0.9 mm of pile head deflection
- SI18-P30 = 1.8 mm of pile head deflection
- SI18-P50 = 2.2 mm of pile head deflection
- SI18-P70 = 1.8 mm of pile head deflection

Assessment:

The previous failure occurred because the slope below the original pile wall slid away leaving the wall unsupported. This resulted in a catastrophic failure of the steel piles, which were severely bent over. High groundwater levels were also a factor. In addition, the backslope inclination was too steep for the clayey soils that were present in it.

The new design added a large toe berm and cut back the backslope to reduce the overall inclination of the combined fill and backslope. A drainage blanket was constructed under the berm to prevent a buildup of groundwater behind the new berm fill. The pile wall was added to protect the new road surface from the existing landslide scarp that was located at the edge of the temporary detour fill. Surface drainage was also controlled by draining the upslope ditch water into a welded SWSP drop pipe, and precipitation and groundwater seepage from the slide mass into a riprap lined swale, both of which were extended down to the terrace at the toe of the valley slope.

The remedial measures appear to be performing well to date. Pile deflections are all within expected ranges and the global stability of the toe berm and backslope slopes look good. Grass is starting to catch on the site and the erosion prevention measures appear to be working.

The slump located above the west riprap channel is likely located in weak native material that had been pre-sheared during landslide events prior to construction. This should be repaired soon before it grows in size.

Recommendations:

Maintenance

The local slump above the west riprap channel should be excavated and replaced with free draining gravel.

It is recommended to inspect this site again next year to better gauge well the site is performing since the remedial measures.































