ALBERTA TRANSPORTATION GEOHAZARD ASSESSMENT PROGRAM PEACE REGION – SWAN HILLS 2022 INSPECTION



Site Number	Location		Name			Hwy		km				
SH001-1 SH001A-1	North of Swan Hills		Swan Hills Retaining Wall			33:12		9.33-9.75 10.00-10.05				
Legal Description			UTM Co-ordinates									
SE/NE05-67-09-W	′5M			11U	E 607,54	15	Ν	6,0)70,516			
			Data		DE	CE.			Total			
		Date						10tai				
Previous Inspect	ion:	10-Jun-2020		SH0014.7		4		21				
		30-May-2022		SH	001-1:9	4		36				
Current Inspection	on:			SH	1001A: 7	3		21				
Road AADT:			11	10		Year:			2022			
		Ris	Rishi Adhikari, T			Ken Froese, Thurber						
Inspected By:		Ed Szmata, TRA		NS		Mark Gallego, Thurber						
mopeoted by.		Ma	x Shannon, T	RANS		Trevor Sterling, Thurber (Safety)		per (Safety)				
		Ro	Rodney Johnston, TRANS			Rob Cottreau, Thurber (GIS)						
		\checkmark	Photographs									
Report Attachme	ents:		Plans			Maintonanco Itoms						
		I.							,			
			SH001-1: Hi	ahwav	embankme	ent placed ov	er cre	ek/au	ully obstructing			
			seepage and	d mobil	lizing slide	with creep n	novem	ents	at about 18 m			
Primary Sito les	.o.	to 20 m d		n depth below the roadway. Pavement distress occurring								
Frinaly Sile 1550	10.		behind and to the south of the floating pile wall.									
			SH001A: Rotational landslide causing vertical displacement of									
			highway surface.									
			SH001-1: The pile wall is ~81 m in length. Pavement distress									
Dimensions:			encompasses approximately 2/0 m of highway.									
			SHUUTA-1: 50 m of highway affected by soft subgrade and slope									
			Site SH001-	1:								
			1970: Highway reconstructed about 30 m from original alignment									
			which was buried by backslope failure.									
			1979: 9 – 50mm dia. slotted steel horizontal subdrains installed 3 m									
			to 7.5 m below the roadway. Subdrain at 3 m depth installed in									
			backslope ditch draining to four culverts.									
Date of Remediation: Maintenance:			<u>1982:</u> Backslope drains no longer functioning; 5 norizontal PVC									
			lengths between 61 m and 73 m									
			1989: Floating concrete pile wall 81 m long installed to depths of 6 m									
			to 12 m below roadway surface. The 82 piles were 760 mm diameter									
			installed at 1 m centre-to-centre spacing.									
			1991: Two rows of tie-back anchors install 1 m and 3 m below top of									
			piles at 30° into clay shale at a length of 7.5 m.									
			<u>1995, 1996:</u> Backslope offloading undertaken.									
			2010: ACP curb installed directing surface water into two "T" drains;									
			sidesiopes regraded and tops of piles covered with gravel; guardrail									
			Site SH001A-1									
			No remediation was done other than patching									
			ACP patching as required to maintain surface (most recent in 2015)									
			2014 and 20	16: T-I	Drains clear	ned out.		2014 and 2016: T-Drains cleaned out				

	2016: Washed rock placed in erosion gullies on sideslope at ea end of guardrail; patch placed to the west of the guardrail. 2018: Installation of three inclinometer/piezometers sets SH001-1 and one set at SH001A-1. 2020: Patching 2022: Patching		
Observations:		Description	Worsened?
Pavement Distress		SH001-1: Cracking present over much of the length; dip south of the wall appeared Spring 2016 and second in 2019. Slight hump near west end of guardrail appeared in 2018 and second in 2019. Tension cracking continues to increase. Lack of maintenance leading to surficial deterioration (potholes). SH001A-1: dips have formed at both ends of patch and hump appeared in 2019; crack pattern is widening and becoming braided.	
Slope Movement		SH001-1: Ongoing creep movement causing cracking and settling of highway surface at south end of pile wall. Slope may be pulling away from pile wall. SI south of wall sheared off in 2 years. SH001A-1: pavements cracks have developed into scarp pattern and are widening with vertical deformation.	N
✓ Erosion		SH001-1: Some erosion noted on sideslope between and below piles. Deeper channels at west end of wall were infilled but are reforming Erosion in east ditch south of wall starting to revegetate; new gully forming in west ditch.	v
✓ Seepage		SH001-1: Seepage observed in backslope area and wet zones noted below the pile wall. SH001A-1: Steady flow observed in east tree line and ditch.	
✓ Bridge/Culvert Distress		SH001-1: T-Drains outlets have been plugged with debris (partially accumulated since last cleaning) and one inlet is slightly damaged. Two sinkholes near the inlet of the culvert north of the pile wall have joined to form a single and larger sinkhole and there are slumps near the outlet. SH001A-1: No apparent distress at culvert 130 m north of site.	V
□ Other			
Instrumentation (as of Spring 2022) – SH001-1:			
SI-16, -18, -20	Have not shown a discernable movement pattern. Likely located outside of the main movement area.		
SH18-4	Located southwest of pile wall. Sheared off at 16.8 m depth after less than two years at a cumulative displacement of 37 mm.		
SI18-5	Located on the upslope of the southwest half of the pile wall. There is movement at about 8.6 m depth with current rate of 1.8 mm/year and a cumulative displacement of 10.5 mm.		
SI18-6	Located on the upslope of the northeast half of the pile wall. No discernable movement pattern.		I. No discernable

PN-1, PN-2, PN-3, PN-4, PN01-2	Measured water levels have been relatively stable for about the last 10 years with minor seasonal variation (typically less than 1 m) noted at the piezometers.		
PN18-4A, 4B, 5A, 5B, 6A, 6B	Slight increasing trend at PN18-4B, -6A, and -6B since installation in March 2018 and the remainder have been relatively stable.		
PN01-1	Not operational.		
Instrumentation (as of Spring 2022) – SH001A-1:			

Instrumentation (as of Spring 2022) – SH001A-1:

SI18-7	Sheared off at 8.5 m after Spring 2019 reading. Cumulative displacement was 50 mm from installation in March 2018.
PN18-7A & 7B	PN18-7A has a slow upward trend and is currently at a historical high of 2.2 m above-ground level; PN18-7B had been trending downward slightly since all 2018 but has now stabilized at 11.3 m BGL.

Assessment:

At SH001-1, the highway embankment crosses two natural gullies which may have had prior instability. The additional weight of the embankment fill combined with blocking springs and natural drainage paths led to movements at this site. The floating pile wall appears to be adequately stabilizing the highway over its length; however, there is some ongoing creep movement and increasing amount cracking and distortion (dips and humps) of the highway at and beyond the southwest end of the wall. New inclinometers installed in March 2018 show movement of the slope south of the wall (SI18-4 has sheared off) and minor movement behind the south half of the wall (SI18-5) but no discernable displacement behind the north half (SI18-6). The drainage control measures implemented in 2010 (asphalt curb and T-down drains) had been functioning though the continued deterioration of the curb and plugging of the drains is currently limiting their functionality (although the drains are occasionally flushed). It was observed that the drains are partially plugged and showing signs of undermining. The piezometers installed in 2018 have identified that the water level behind the wall is approximately 4 m lower than in the unstable ground to the south of the wall.

The highway surface south of the wall was patched over, which covered the previous cracks and potholes observed from the 2020 inspection. However, the cracks have started to reflect through the patched area and potholes are forming, especially in the southbound lane. There continues to be minor increases in the crack length, width, and frequency beyond both ends of the wall. The two sinkholes at the culvert inlet north of the wall have joined together to form a larger sinkhole that likely extends right down the culvert. The scarp previously observed at the outlet was still present with some indication that it might be located over an abandoned culvert outlet. Apparent movement of the soil downslope of the pile wall has further opened up tension cracks between and below some of the piles. The absence of movement at SI18-6 would indicate that this movement is occurring downslope of the wall rather than through it. Although the scarp features located northwest of SI16 through SI21 are not new (they are apparent on 2007 LiDAR), it was noted this year that there appeared to be more movement since 2020, which will need to be monitored in future visits. The SI's between the 2007 scarps and the highway do not yet indicate movement.

Site SH001A-1 was first observed in 2013 after an FWD (falling weight deflectometer) program. The distress consists of cracking with associated dips in the pavement surface and has required patching in 2014 and 2015. It was initially suspected that the underlying issue was a soft/wet subgrade possibly associated with shallow groundwater flow. This is plausible as this location is on the flank of a small channel passing through a culvert (600mm diameter smooth-wall steel-lined at km 10.156) approximately 120 m to the northeast and the terrain to the northwest appeared to be wetter than surrounding areas. In 2017, the site inspection was conducted shortly after heavy rainfall and it was observed that there was significant flow (northeast toward a centreline culvert) in the east ditch but within the treeline, which has continued to be the case in all subsequent visits. By 2018, the crack pattern across the highway had developed into a landslide scarp and the movement zone in the inclinometer (which sheared off after the Spring 2019 readings) confirmed there is slope movement at this location at a depth of 8 m. The crack pattern lines up with the 0.5 m scarp feature observed to the west of the highway. Thus, the soft/wet subgrade may be a result of slope displacement and resultant

modified groundwater flow regime. Like at SH001-1, the highway was patched in 2022 but the cracks and potholes are starting to surface through the patch. The soil stratigraphy observed in SH18-7 consists of gravel and clay fill overlying native clay over a thin zone of clay till. The site is underlain by clay shale with sandstone layers. The movement zone appears to be at the contact between the clay till and clay shale. The high groundwater level measured in the clay till layer, which became artesian in Spring 2019, might be a trigger for the slide movements. The Spring 2022 readings still indicate flowing artesian groundwater conditions. The mechanism for the landslide occurring at this site has not yet been identified. There is about 20 m of relief from the highway surface to the downslope creek but over a distance of about 190 m which is relatively flat (6°); however, remolded shale is expected to have a low friction angle.

Recommendations:

Short-Term:

- Road maintenance should continue as necessary to maintain the roadway surface and may consist of milling, patching, and crack sealing of the ACP.
- Re-establish the asphalt curb and clean the T-drains (this should be a periodic maintenance item).
- Re-grade, and augment with additional granular material, if necessary, the sideslope below the pile wall as was partially undertaken since the 2016 inspection.

Medium Term

SH001A: An inexpensive option would be to install a subdrain in the upslope ditch to see if intercepting some of the groundwater might reduce the rate of movement. Although this is unlikely to remediate the site, it might extend the time before a full intervention is necessary.

Long-Term:

SH001-1: Consideration should be given to placing additional horizontal drainage measures to further reduce groundwater levels in the highway embankment particularly to the southwest of the wall. This might also be accomplished with a subdrain or relief wells to the south of the highway. Consideration could also be given to extending the pile wall further southwest should ongoing maintenance become difficult and/or expensive.

SH001A-1: With confirmed movement at this site, it is recommended that a preliminary engineering assessment be undertaken to determine potential mechanisms and develop alternates for stabilizing this location. A LiDAR review should be included to try to better define the possible limits of the landslide.

Ongoing Investigation:

It is recommended that the annual Geohazard inspection should continue as scheduled.

Closure:

It is a condition of this letter report that Thurber's performance of its professional services will be subject to the attached Statement of Limitations and Conditions.

Renato Clementino, P.Eng. Principal | Senior Geotechnical Engineer

Mark Gallego, P.Eng. Geotechnical Engineer



STATEMENT OF LIMITATIONS AND CONDITIONS

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This Report has been prepared in accordance with generally accepted engineering or environmental consulting practices in the applicable jurisdiction. No other warranty, expressed or implied, is intended or made.

2. COMPLETE REPORT

All documents, records, data and files, whether electronic or otherwise, generated as part of this assignment are a part of the Report, which is of a summary nature and is not intended to stand alone without reference to the instructions given to Thurber by the Client, communications between Thurber and the Client, and any other reports, proposals or documents prepared by Thurber for the Client relative to the specific site described herein, all of which together constitute the Report.

IN ORDER TO PROPERLY UNDERSTAND THE SUGGESTIONS, RECOMMENDATIONS AND OPINIONS EXPRESSED HEREIN, REFERENCE MUST BE MADE TO THE WHOLE OF THE REPORT. THURBER IS NOT RESPONSIBLE FOR USE BY ANY PARTY OF PORTIONS OF THE REPORT WITHOUT REFERENCE TO THE WHOLE REPORT.

3. BASIS OF REPORT

The Report has been prepared for the specific site, development, design objectives and purposes that were described to Thurber by the Client. The applicability and reliability of any of the findings, recommendations, suggestions, or opinions expressed in the Report, subject to the limitations provided herein, are only valid to the extent that the Report expressly addresses proposed development, design objectives and purposes, and then only to the extent that there has been no material alteration to or variation from any of the said descriptions provided to Thurber, unless Thurber is specifically requested by the Client to review and revise the Report in light of such alteration or variation.

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5. INTERPRETATION OF THE REPORT

- a) Nature and Exactness of Soil and Contaminant Description: Classification and identification of soils, rocks, geological units, contaminant materials and quantities have been based on investigations performed in accordance with the standards set out in Paragraph 1. Classification and identification of these factors are judgmental in nature. Comprehensive sampling and testing programs implemented with the appropriate equipment by experienced personnel may fail to locate some conditions. All investigations utilizing the standards of Paragraph 1 will involve an inherent risk that some conditions will not be detected and all documents or records summarizing such investigations will be based on assumptions of what exists between the actual points sampled. Actual conditions may vary significantly between the points investigated and the Client and all other persons making use of such documents or records with our express written consent should be aware of this risk and the Report is delivered subject to the express condition that such risk is accepted by the Client and such other persons. Some conditions are subject to change over time and those making use of the Report should be aware of this possibility and understand that the Report only presents the conditions at the sampled points at the time of sampling. If special concerns exist, or the Client has special considerations or requirements, the Client should disclose them so that additional or special investigations may be undertaken which would not otherwise be within the scope of investigations made for the purposes of the Report.
- b) Reliance on Provided Information: The evaluation and conclusions contained in the Report have been prepared on the basis of conditions in evidence at the time of site inspections and on the basis of information provided to Thurber. Thurber has relied in good faith upon representations, information and instructions provided by the Client and others concerning the site. Accordingly, Thurber does not accept responsibility for any deficiency, misstatement or inaccuracy contained in the Report as a result of misstatements, omissions, misrepresentations, or fraudulent acts of the Client or other persons providing information relied on by Thurber. Thurber is entitled to rely on such representations, information and instructions and is not required to carry out investigations to determine the truth or accuracy of such representations, information and instructions.
- c) Design Services: The Report may form part of design and construction documents for information purposes even though it may have been issued prior to final design being completed. Thurber should be retained to review final design, project plans and related documents prior to construction to confirm that they are consistent with the intent of the Report. Any differences that may exist between the Report's recommendations and the final design detailed in the contract documents should be reported to Thurber immediately so that Thurber can address potential conflicts.
- d) Construction Services: During construction Thurber should be retained to provide field reviews. Field reviews consist of performing sufficient and timely observations of encountered conditions in order to confirm and document that the site conditions do not materially differ from those interpreted conditions considered in the preparation of the report. Adequate field reviews are necessary for Thurber to provide letters of assurance, in accordance with the requirements of many regulatory authorities.

6. RELEASE OF POLLUTANTS OR HAZARDOUS SUBSTANCES

Geotechnical engineering and environmental consulting projects often have the potential to encounter pollutants or hazardous substances and the potential to cause the escape, release or dispersal of those substances. Thurber shall have no liability to the Client under any circumstances, for the escape, release or dispersal of pollutants or hazardous substances, unless such pollutants or hazardous substances have been specifically and accurately identified to Thurber by the Client prior to the commencement of Thurber's professional services.

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LEGEN	D		
<u></u>	SCARP (INTERPRETED FROM LIDAR)		
-	SLOPE INCLINOMETER (APPROXIMATE)		
×	DESTROYED SLOPE INCLINOMETER		
	APPROXIMATE INSTRUMENT LOCATION (2018)		
PN	PNEUMATIC PIEZOMETER		
SI	SLOPE INCLINOMETER		
	GULLY		
	DRAINAGE PATHS (INTERPRETED FROM LIDAR)		
-00	GUARDRAIL		
\sim	TREE LINE		
٠	RED TEMPORARY HAZARD SIGN		
07	DIRECTION AND NUMBER OF PHOTO		
1. FEA 2. LID/ 0° T 3. PRE 4. MA1 5. DRA IMA	TURE LOCATIONS ARE APPROXIMATE. AR SHADED ACCORDING TO SLOPE FROM WHITE AT O BLACK AT 35° AND STEEPER. WIOUS OBSERVATIONS SHOWN IN BLACK. (2022 OBSERVATIONS SHOWN IN RED. WING UPDATED IN 2017 USING LIDAR, SATELLITE GERY, AND A MEASURING WHEEL.		
(<u>20 40 60 80 m</u>		
	SCALE 1:1500		
ROVIDED BY	ALBERTA TRANSPORTATION (FLOWN 2007)		
Alberta			
PEACE REGION (SWAN HILLS)			
SH001-1: HWY 33:12 2022 SITE INSPECTION PLAN			
	DWG No. 32121-SH001-1		

DRAWN BY	ML
DESIGNED BY	KEF
APPROVED B	RVC
SCALE	1:1500
DATE	SEPTEMBER 2022
FILE No.	32121





<u>LEGEND</u>

\sim	CRACK
	WATER COURSE
-	APPROXIMATE INSTRUMENT LOCATION (2018)
PN	PNEUMATIC PIEZOMETER
SI	SLOPE INCLINOMETER
17	DIRECTION AND NUMBER OF PHOTO

<u>NOTE</u>S

- 1. FEATURE LOCATIONS ARE APPROXIMATE.
- 2. PREVIOUS OBSERVATIONS SHOWN IN BLACK (2013-2015 FROM AMEC FIGURE 1, PROJECT EG10030, PROVIDED BY ALBERTA TRANSPORTATION).
- 3. CRACK PATTERN REDRAWN AFTER PATCHES PLACED IN 2020 AND 2022.
- 4. MAY 2022 OBSERVATIONS SHOWN IN RED

7.5 10 12.5 15 m 2.5 5 SCALE 1:250

Alberta PEACE REGION (SWAN HILLS) SH001A-1: HWY 33:12 2022 SITE INSPECTION PLAN DWG No. 32121-SH001A-1 RAWN BY ML DESIGNED BY KEF PPROVED BY RVC SCALE 1:250 DATE SEPTEMBER 2022 THURBER ENGINEERING LTD. FILE No. 32121





Photo 1, SH001-1 – Looking southwest at patch over cracks forming at the southwest end of the wall .



Photo 2, SH001-1 – Looking north at cracking in highway surface immediately south of the pile wall.





Photo 3, SH001-1 – Looking southwest at scarp on slope below highway between SI20 and SI21.



Photo 4, SH001-1 – Looking southwest at scarp below highway near SI18.





Photo 5, SH001-1 – Looking south at erosion in east ditch.



Photo 6, SH001-1 – Looking south at cobbles placed in gully at north end of guardrail.





Photo 7, SH001-1 – Looking southwest at cracked curb at south end of guardrail.



Photo 8, SH001-1 – Seepage out of slope below north-most T-drain.





Photo 9, SH001-1 – Erosion and/or movement away from the piles around the southwest down drain.



Photo 10, SH001-1 – Soil pulling away from the downslope side of piles near the northwest downdrain.





Photo 11, SH001-1 – 920 mm dia. centreline culvert outlet.



Photo 12, SH001-1 – Two sinkholes at culvert inlet have combined to form a larger sinkhole.





Photo 13, SH001A-1 – Crack pattern at the north end of the Site.



Photo 14, SH001A-1 - Looking northeast from the south end of the patch.





Photo 15, SH001A-1 – Looking northeast at roadway crack and scarp (red line) at tree line.



Photo 16, SH001A-1 - Looking west at cracks at south end of patch.