ALBERTA TRANSPORTATION GEOHAZARD ASSESSMENT PROGRAM PEACE REGION – HIGH LEVEL 2017 INSPECTION



Site Number	Locatio	n		Name			Hwy	km	
PH045-1 North of Mann			ing, AB	Meikle River (Pile Wall)			35:08	26.2	
Legal Descripti		C :	UTM Co-ordinates			·			
SW7-94-22-W5M 11U E 467,581 N 6,333,081									
			Date	PF		CF		Total	
Previous Inspection: 11		11-	June-2015	10		4		40	
Current Inspection:		21-	June-2017	7		4		28	
Road AADT:		1720			Year:		2014		
			er Skirrow, TI zmata, TRAN		Ken Froese, Don Proudfo				
Report Attachments:		P	hotographs	Plans		🗖 Mainte		enance Items	
Primary Site Issue: Slope movement and erosion affecting highway and sideslope								nd sideslope	
Dimensions:			115 m pile wall						
Date of Remediation:			2016: Install H-pile and lagging formwork to backfill around existing cap beam with fillcrete; highway overlaid; new guardrail installed						
Maintenance:			2011: Pitrun placed to repair erosion at drain and repair elephant trunk Frequent patching of voids behind cap beam						
Observations:			Description					Worsened?	
Pavement Distress			Had been cracking and voids against pile wall; these were excavated and filled with grout						
Slope Movement			North slide graben relatively unchanged since 2015						
Erosion			Erosion beneath wall and around drain pipes repaired;						
✓ Seepage			Pile wall voids repaired; subdrain pipe in lower portion of slope exposed and extended						
Bridge/Culvert Distress									
Other			Sheet metal cover covering H-piles and timber lagging damaged by wind					V	
Instrumentation (as of Fall 2017):									
Destroyed	SP10-2, 3, and -5 and VW10-1 and -2 were destroyed before or during constructio in 2015.							ring construction	
Inclinometers	Three slope inclinometers (SI-49, -50 and -51) within the cap beam remain operational. Cumulative pile head movements are currently 66 mm to 149 mm with rate of movement of 2.2 mm/year to 5.0 mm/year which are similar to the previous few readings. Rate plots show continued movement in all three SI's corresponding to deflection of the cap beam with no immediately obvious effect from the recent repairs.								
Assessment:									
Site is subjected to ongoing creep movements of the slope which had been leading to the formation of voids behind the pile wall and cap beam and subsequent loss of material from below the highway and cap beam. During construction it was observed that the tie-back anchors shown on the drawing consisted of 100 mm diameter screw piles drilled at various depths and angles and are free-floating (not connected to the piles or cap beam). These anchors perhaps provide some minimal reinforcement of the slope but do not contribute to holding the wall in place. The excavation behind									

the cap beam to clean out the voids was between 1.5 m to 2 m in width and 527 m³ of grout was required to backfill the excavation. During excavation, there was a hard ledge of asphalt encountered about 1 m below the top of the cap beam from about 30 m to 57 m south of the north end of the cap beam that required an excavator-mounted jackhammer to break up. The pattern of highway surface repairs indicates that that area was likely the lowest point of previous failures. At some point, a base sandwich was required to repair the highway surface. It should be noted that the cap beam had variable thickness being 2 m on the face (downslope) and 1 m on the back (upslope) with the vertical transition occurring near the face downslope of the capped concrete piles.

The repairs undertaken to the wall were to protect against future void formation rather than to provide additional support against movement. It is anticipated that the wall will continue to deflect due to the creep movement of the slope. However, having grout adjacent to and below the cap beam should inhibit erosion and the subdrain installed below the highway GBC against the cap beam should capture and channel water better than occurred in the past.

Recommendations:

Short-Term:

Repair the flashing along the top of the timber lagging wall. It may be possible to salvage some of the pieces. It is recommended that a sealant be used against the concrete and that more frequent sheet metal screws with larger washers be used to secure the flashing. It is also recommended that the bottom edge of the flashing be screwed or bolted to the timber lagging, particularly at the overlap of adjacent pieces, to provide additional resistance against wind.

Long-Term:

 It may become necessary to install tie-backs to limit movement of the wall to avoid failing the piles. A geotechnical investigation and analysis of pile-soil interaction will be necessary to design the tieback system.

Ongoing Investigation:

 It is suggested that the annual GeoHazard inspections be carried out at least one more year and that bi-annual instrumentation readings should continue as scheduled.

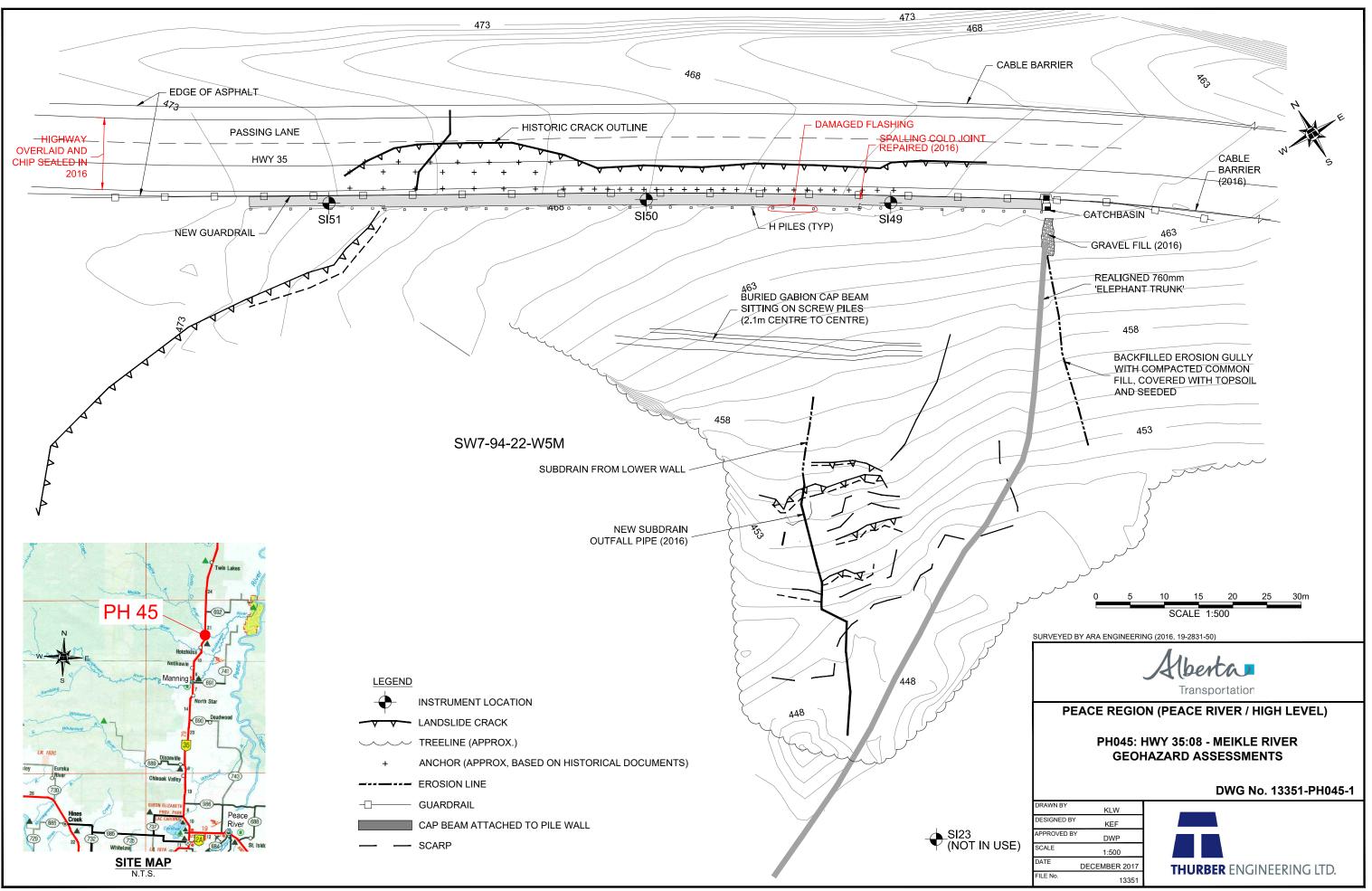








Photo 1 – Looking northwest at catch basin and pile wall.



Photo 2 – Catch basin inlet at south end of wall leading to the elephant trunk downpipe.







Photo 3 – Looking downslope at "elephant trunk" drain pipe.



Photo 4 – Looking northwest at repaired and overlaid asphalt surface. Note new bridge rail installed along the top of the cap beam and damaged flashing at about the center of the wall.







Photo 5 – Looking northwest at main section of damaged flashing.



Photo 6 – Looking southeast at repaired and overlaid asphalt surface. Note new bridge rail installed along the top of the cap beam.







Photo 7 – Looking northeast at subdrain in the lower part of the slope that was located and extended during 2016 construction.



Photo 8 – Looking north at graben block northwest of the wall.







Photo 9 – From the north end looking east at pile wall with scarp in foreground.