ALBERTA TRANSPORTATION GEOHAZARD ASSESSMENT PEACE REGION (PEACE RIVER DISTRICT) 2022 INSPECTION



Site Number	Location			Name	Hwy		km		
PH045-1 North of Manr		ing, AB	AB Meikle River (Pile Wa		35:08	3 26.2			
Legal Description UTM Co-ordinates									
SW7-94-22-W5M			11U E 467,581		581	N 6,333,081			
			Date	ate PF CF			Total		
Previous Inspection:		21-June-2017		7	4	4		28	
Current Inspection:		3-June-2022		11	4		44		
Road AADT:		133		30	Year:		2022		
Inspected By:		Rishi Adhikari, TRANSKen Froese, ThurberEd Szmata, TRANSMark Gallego, ThurberMax Shannon, TRANSErwin Kurz, TRANS					er ber		
Report Attachments:		Photographs		✓ Plans	Plans 🗖 Mainte		enance Items		
Primary Site Issue: Slope movement and erosion affecting highway and sideslope								sideslope	
Dimensions:			115 m pile wall						
Date of Remediation:			2016: Install H-pile and lagging formwork to backfill behind and below existing cap beam with fillcrete; highway overlaid; new HTSC guardrail installed 2018: HTSC replaced by W-Beam guardrail						
Maintenance:			2011: Pitrun placed to repair erosion at drain and repair elephant trunk Frequent patching of voids behind cap beam						
Observations:			Description				Worsened?		
Pavement Distress			Pile wall starting to pull away again – crack opening up against waler						
Slope Movement			North slide graben starting to move (2022) and taking lagging wall with it.					2	
Erosion			Erosion beneath wall and around drain pipes repaired;						
✓ Seepage			Pile wall voids repaired; subdrain pipe in lower portion of slope exposed and extended						
Bridge/Culvert Distress									
✓ Other			H-piles and timber lagging damaged by slope movement and pulling away from the waler					•	
Instrumentation (as of Spring 2022):									
Inclinometers Inclinometers (SI-49, -50 and -51) within the cap beam remain operational. Cumulative pile head movements are currently 73 mm to 160 mm with rates of movement of 2.8 mm/year to 5.7 mm/year, which are similar to the previous few readings. Rate plots show steady movement at SI-49, accelerating trend at SI-50, and variable trend at SI-51 (but with overall steady trend) with no obvious long-term improvement from the 2016 repairs.									
Assessment:									

The site is subjected to ongoing creep movements of the slope had led to the formation of voids behind the pile wall and cap beam and subsequent loss of material from below the highway and cap

beam. This was repaired in 2016 using steel H-piles and timber lagging to act as forms for placement of grout in the voids. During construction, it was observed that the tie-back anchors shown on the drawing consisted of 100 mm diameter screw piles installed at various depths and angles and are free-floating (not connected to the piles or cap beam). These anchors perhaps provide some minimal reinforcement of the slope but do not contribute to holding the wall in place. The excavation behind the cap beam to clean out the voids was between 1.5 m to 2 m in width and 527 m³ of grout was required to backfill the excavation. During excavation, there was a hard ledge of asphalt encountered about 1 m below the top of the cap beam from about 30 m to 57 m south of the north end of the cap beam that required an excavator-mounted jackhammer to break up. The pattern of highway surface repairs exposed during excavation indicates that that area was likely the lowest point of previous failures. At some point, a base sandwich was required to repair the highway surface. It should be noted that the cap beam had variable thickness being 2 m on the face (downslope) and 1 m on the back (upslope), with the vertical transition occurring near the face downslope of the capped concrete piles.

The repairs undertaken to the wall were to protect against future void formation rather than to provide additional support against movement. It was anticipated that the wall would continue to deflect due to the creep movement of the slope. At the time of 2022 assessment, this creep movement has resumed resulting in the displacement of two sections of the timber lagging wall, formation of a void below the cap beam, and fresh displacement on the scarp and graben at the north end of the wall. The orthophoto developed from drone photography allowed the identification of several additional scarps forming below the wall. Unfortunately, the crack between the asphalt and the cap beam has started forming again. It appears that the landslide has begun active movement, i.e., more than creep, and there is the potential for significant displacement particularly at the north end of the site.

Recommendations:

Short-Term:

• Routine crack sealing between the asphalt and the cap beam to limit infiltration of runoff.

Long-Term:

 As this landslide has become active again, it is recommended that a geotechnical investigation and analysis of pile-soil interaction be undertaken in the near-future so that a tie-back system can be designed. It is anticipated that additional stabilization measures will be required at this site.

Ongoing Investigation:

• Due to the recent movement, it is suggested that the frequency of Geohazard inspection be increased to at least every second year. Bi-annual instrumentation readings should continue as scheduled.

Closure

It is a condition of this letter report that Thurber's performance of its professional services will be subject to the attached Statement of Limitations and Conditions.

Renato Clementino, Ph.D., P.Eng. Principal | Senior Geotechnical Engineer

Ken Froese, P.Eng. Associate | Senior Geotechnical Engineer



STATEMENT OF LIMITATIONS AND CONDITIONS

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This Report has been prepared in accordance with generally accepted engineering or environmental consulting practices in the applicable jurisdiction. No other warranty, expressed or implied, is intended or made.

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- d) Construction Services: During construction Thurber should be retained to provide field reviews. Field reviews consist of performing sufficient and timely observations of encountered conditions in order to confirm and document that the site conditions do not materially differ from those interpreted conditions considered in the preparation of the report. Adequate field reviews are necessary for Thurber to provide letters of assurance, in accordance with the requirements of many regulatory authorities.

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CABLE BARRIER - CRACK AT CAP BEAM 20mm-WIDE, 40mm DEEP NEW W-BEAM GUARDRAIL (2016) CATCHBASIN 463 GRAVEL FILL (2016) ULLY FORMING IN RUT (2022) REALIGNED 760mm 'ELEPHANT TRUNK' 458 BACKFILLED EROSION GULLY WITH COMPACTED COMMON FILL, COVERED WITH TOPSOIL AND SEEDED 453 SURVEYED BY ARA ENGINEERING (2016, 19-2831-50); ORTHOIMAGE BY THURBER FROM DRONE IMAGERY FLOWN JUNE 2, 2022 Alberta PEACE REGION (PEACE RIVER / HIGH LEVEL) PH045: HWY 35:08 - MEIKLE RIVER **GEOHAZARD ASSESSMENTS** DWG No. 32121-PH045-1 AWN BY ML DESIGNED B KEF ROVED DWP CALE 1:500 OCTOBER 2022 THURBER ENGINEERING LTD. 3212⁻



Photo 1 – Looking northwest at the catch basin and pile wall.



Photo 2 – Catch basin inlet at the south end of the wall leading to the elephant trunk downpipe.



Photo 3 – Looking downslope at "elephant trunk" drain pipe. There is some erosion forming in mower ruts on the left (south) side of the drain pipe.



Photo 4 – Looking northwest at repaired and overlaid asphalt surface. A new bridge rail was installed during construction and damaged flashing at about the center of the wall noted previously has been repaired.



Photo 5 – Looking north at the displaced H-pile and timber lagging wall near the scarp at the north end of the wall.



Photo 6 – Looking east at the end of the displaced section of lagging and beyond to (as yet) undisturbed lagging.



Photo 7 – Looking at the crack that is opening up again between the cap beam and asphalt.



Photo 8 – Looking west at graben block northwest of the wall, which appears to have become reactivated.



Photo 9 – The crack forming below the lagging wall at the south end where the soil is starting to pull away.



Photo 10 – The void forming in front of and behind the cap beam as the lagging wall and grout backfill is displaced by slope movement.