# ALBERTA TRANSPORTATION GEOHAZARD ASSESSMENT PROGRAM PEACE REGION (PEACE RIVER DISTRICT) 2022 INSPECTION



Site Number	Location	ocation		Name		Hwy	km		
PH034 Judah Hill		l	Fence Slide			744:04	59.177		
Legal Description				UTM Co-ordinates					
SE¼ 29-083-21 W5M				11V E 482792 N 6230946			46		
			Date	Date BE CE		Total			
Previous Inspection:		6- July-2021		14	5	70			
Current Inspections:		0-July-2021		14	5	70			
Road WAADT:		24-1viay-2022		20	Year:		2021		
		Tvle	vier Clay TEI Don Proudfoot TEI				-021		
Inspected by:		Ed	Szmata TRA	NS Roger Skirrow, TRANS					
		Max	Max Shannon, TRANS						
Report Attachments:									
			Plans	nce Items	\$				
Primary Site Issu	le:		An approximately 50 m wide slide, with its backscarp within the						
			some old sto	palled in 2005 by	I rebuilding the b	iahway w	ith geogrid		
			some ou stone columns) and repulling the highway with geogra						
			pavement have occurred and cracks have extended further south						
			and north of the original slide.						
Dimensions:			Main slide is about 60 m wide at the road shoulder. Additional areas						
			of pavement distress and cracking extend 80 m to 100 m north and						
			south of the main slide.						
Maintenance:			Cracking and dips in pavement were patched in 2008 and again in						
			2011. Patching has occurred intermittently following these repairs						
			and both the guardrail and posts were replaced in 2009. Highway						
			was closed between May 2013 and December 2013 due to the						
			south						
Observations:			Description			Wors	ened?		
			Near km 59.	1 (near SI10-12),	subsidence with	in			
			the SBL near the guardrail is up to 150 mm. No			lo			
			significant expansion or change from 2021.			1.			
			(Photo 1)						
			Existing cracks in the SBL shoulder near km						
			59.13 did not change significantly since 2021.						
Pavement Distress			At the main	repair area (km 5	9.14) the cracks i	in			
			the SBL shoulder are worse and are open up to			~			
			100 mm. The depression has a differential drop up to 350 mm with a sharp differential edge in the ACP that is worse from the previous inspection						
			ın 2021. (Ph	otos 2 and 3)					
			Pavement condition at km 59.2 had no significant						
			change from 2021. (Photo 6)						
			enange nom						
K Slope Mayrement		At main s	lide repair area	a: the previous	ly				
Siope iviovement			observed sh	allow slump and	skin failure in th	ne			

		clay cap that was constructed over the sideslope during the 2005 repairs had no changes. Except for surficial erosion, slope appears similar to 2021 condition. (Photo 4)				
		A shallow and dry earth slide was noted below SI10-15 on the west sideslope (km 59.25). (Photo 7)				
Erosion		Increased rill erosion is present in the upper sideslope at the main slide repair area (km 59.18).				
Seepage						
Bridge/Culvert Distress						
Other		Geogrid installed as part of the 2005 repair has been previously observed becoming exposed on the embankment downslope resulting in a further reduction of its anchoring capacity.				
Instrumentation:						
SI05-15	Slope inclinometer installed in 2005 at the top of the hill in the ATCO gas utility right of way above the Fence Slide, approximately 30 m elevation above the road, has not shown any consistent trend of movement since installation.					
SI10-12 and 15	The Spring 2021 readings for SI10-15 showed a rate of movement of 4.4 mm/yr over 2.4 m to 5.5 m depth. The rate of movement in SI10-15 has shown a generally steady trend since initialization and has typically been between 2 to 7 mm/yr. SI10-12 sheared at 4.9 m depth in Fall 2019.					
SI10-13 and 14	SI10-13 and SI10-14 are obstructed at depths of 6.4 m and 5.7 m, which correspond to the approximate elevation of the base of the upper clay fill of the 2005 repair.					
PN10-12 and 15	Pneumatic piezometers PN10-12 and PN10-15 showed decreases in groundwater level of 0.04 m and 0.05 m, respectively, since the fall of 2021 readings. The equivalent piezometric depths have shown generally steady trends since initialization in 2010.					
PN10-13 and 14	and 14 Non-Operational (Pinched or Blocked).					
A						

# Assessment:

Cracking and settlement at the repair have continued, and cracking is re-appearing through the 2011 asphalt patch and continues to worsen along the road shoulder to the north and south of the main slide. The shearing or buckling of SI10-13 and SI10-14 indicate that slide movement or settlement is occurring at a steady rate in the clay backfill from the 2005 repair. SI10-12, located to the south outside the former landslide repair limits, showed a steady annual rate of movement of about 8 mm/yr up until it sheared off in Fall 2019. The movement measured at SI10-15, located north of the slide repair area, is at a rate of about 5 mm/yr (highest movement rate of 11 mm/yr was recorded in the fall of 2020).

It is postulated that the dipping in the highway pavement surface is the result of the clay fill settling and spreading over time. The shallow sloughing of the clay cap is considered due to the loss of cohesion as a result of weathering (wetting and desiccation cycles). The repaired sideslope is over-steepened and lateral spreading of the clay fill is expected to continue. The shear depth of the SI's correlates with this assessment.

The development of additional cracks in the highway shoulder south and north of the Fence Slide (in the vicinity of SI10-12 and SI10-15) within the last few years are getting worse and likely indicate potential slope failures at these locations in the southbound lanes in the future. No toe bulge or other visible slide features have been apparent on the slope below the road in recent inspections.

Rill erosion and scouring below the highway SBL resulting from the concentrated water runoff in the lower dipped sections also needs to be addressed as it can lead to progressively larger erosion gullies, skin failures and landslide features, which could eventually retrogress into the roadway.

To reduce maintenance effort along this section of the road it is understood that AT is converting the ACP to a gravel surface between KM 58.480 to KM 59.540 so that any ongoing settlement or slide movements that distort the road surface can be graded out until a more permanent solution is implemented. As part of this work ditch erosion design repairs have also been provided by Thurber between approximately KM 58.5 KM to KM 59.525. Ditch erosion repair designs consist of adding Class 1M riprap to ditch areas already filled with rock, regrading and adding Class 1M over geotextile, TRM with synthetic ditch barriers, and adding riprap bowls. This work is anticipated to be complete by end of October 2022.

Recommendations:	Cost					
A short-term solution for the shallow skin failures in the clay cap over the sideslope is to seed and cover the sideslope with Macmat and anchor it into the slope with Duckbill anchors.	\$75,000					
Mid-term to long term solutions would involve excavating and removing the upper clay backfill from the 2005 repair and rebuilding the highway embankment with granular fill reinforced with uniaxial geogrid, the reinstatement of the clay cap on the embankment sideslope and the placement of an overlying slope protection (Armormax anchored with Duckbill anchors).	\$ 300,000					
Long-term solutions to deal with the propagation of cracks to the north and south of the Fence Slide could consist of a realignment of the highway into the backslope (now that the natural gas pipeline is decommissioned), digging out weaker clay layers and rebuilding the slope with geogrid reinforced gravel (like the Fence Slide repair from 2015) or pile walls. The cost could range from \$2,000,000 to \$10,000,000. The realignment is likely the cheapest option but will only buy some time until further retrogression occurs whereas the pile wall or dig and replace options should be a more permanent solution.	\$2M - \$10M					
Closure:						
It is a condition of this letter report that Thurber's performance of its professional services will be subject to the attached Statement of Limitations and Conditions.						
Don Proudfoot, P.Eng. Principal   Senior Geotechnical Engineer						
Tyler Clay, P.Eng. Geological Engineer						



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- b) Reliance on Provided Information: The evaluation and conclusions contained in the Report have been prepared on the basis of conditions in evidence at the time of site inspections and on the basis of information provided to Thurber. Thurber has relied in good faith upon representations, information and instructions provided by the Client and others concerning the site. Accordingly, Thurber does not accept responsibility for any deficiency, misstatement or inaccuracy contained in the Report as a result of misstatements, omissions, misrepresentations, or fraudulent acts of the Client or other persons providing information relied on by Thurber. Thurber is entitled to rely on such representations, information and instructions and is not required to carry out investigations to determine the truth or accuracy of such representations, information and instructions.
- c) Design Services: The Report may form part of design and construction documents for information purposes even though it may have been issued prior to final design being completed. Thurber should be retained to review final design, project plans and related documents prior to construction to confirm that they are consistent with the intent of the Report. Any differences that may exist between the Report's recommendations and the final design detailed in the contract documents should be reported to Thurber immediately so that Thurber can address potential conflicts.
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# Photo 7.

View of old slump in the backslope near km 59.3. Fresh soil visible in the upper scarp since the 2021 condition.